

On Classical and a Gradient Model of Finite Viscoplasticity

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Outline

- **Phenomenological models with plastic flow co-axial with elastic stretch**
 - **General Theory**
 - **Finite Element Numerics**

- **Crystal Plasticity (with ‘Simple’ Gradient Hardening)**
 - **General Theory**
 - **Finite Element Numerics**
 - **Results**
 - **Polycrystal size effects**
 - **Cleavage of ductile materials**
 - **Orientation dependence of Fracture**

Finite Phenomenological Viscoplasticity

■ Constitutive Description

- Elasticity – Isotropic Hyperelasticity
- Rate Dependent
- Strain Hardening

■ Finite Element Implementation

- Multiplicative Decomposition of Deformation Gradient
- Plastic flow coaxial with elastic stretch
- Rate-independent case is a trivial (one line) modification
- Recovers fully-nonlinear hyperelastic response in the absence of inelasticity
- Nonlinear Viscoelasticity is a straightforward modification

Constitutive Model

Multiplicative Decomposition

$$\mathbf{F} = \mathbf{F}^e \mathbf{F}^p$$

Free Energy/vol

$$\psi = \psi(\mathbf{C}^e)$$

Cauchy Stress

$$\mathbf{T} = \mathbf{F}^e \frac{\partial \psi}{\partial \mathbf{C}^e} \mathbf{F}^{eT}$$

Flow-rule
(No plastic spin)

$$\mathbf{F}^e \dot{\mathbf{F}}^p \mathbf{F}^{p-1} \mathbf{F}^{e-1} = \dot{\gamma} \frac{\mathbf{T}^{dev}}{\|\mathbf{T}^{dev}\|}$$

Rate-Dependence

$$\dot{\gamma} = p(\gamma, \sigma^s) \quad ; \quad \sigma^s = \|\mathbf{T}^{dev}\| / \sqrt{2}$$

Material Update

Kinematics

$$\text{for any } \mathbf{F}_{(\cdot)} \quad \mathbf{C}_{(\cdot)} = \sum_A (\lambda_{(\cdot)}^A)^2 \mathbf{N}_{(\cdot)}^A \otimes \mathbf{N}_{(\cdot)}^A \quad ; \quad \mathbf{n}_{(\cdot)}^A = \mathbf{F}_{(\cdot)} \mathbf{N}_{(\cdot)}^A / \lambda_{(\cdot)}^A$$

Isotropy

$$\mathbf{T} = \sum_A \sigma^A \mathbf{n}_e^A \otimes \mathbf{n}_e^A$$

Flow Rule

$$\mathbf{F}^e \dot{\mathbf{F}}^p \mathbf{F}^{p-1} \mathbf{F}^{e-1} = \frac{\dot{\gamma}}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{n}_e^A \otimes \mathbf{n}_e^A$$

$$\Rightarrow \dot{\mathbf{F}}^p = \frac{\dot{\gamma}}{\sqrt{2}\sigma^s} \left(\sum_A S^A \mathbf{N}_e^A \otimes \mathbf{N}_e^A \right) \mathbf{F}^p \quad ; \quad S^A := A^{\text{th}} \text{ e-value of } \mathbf{T}^{\text{dev}}$$

$$\mathbf{F}^p = \exp \left(\frac{\Delta\gamma}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{N}_e^A \otimes \mathbf{N}_e^A \right) \mathbf{F}_n^p \quad ; \quad \Delta\gamma = \dot{\gamma} \Delta t$$

Discrete Update

Formula

Weber & Anand, 1990

$$\text{Note: } \mathbf{F}_0^p = \mathbf{I} \Rightarrow \det(\mathbf{F}^p) = 1$$

$$\text{since } \det[\exp(\cdot)] = \exp(\text{tr}(\cdot))$$

Material Update

Elastic predictor

$$\mathbf{F}^e = \mathbf{F}\mathbf{F}^{p-1} = \mathbf{F}' \exp\left(\frac{-\Delta\gamma}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{N}_e^A \otimes \mathbf{N}_e^A\right) ; \quad \mathbf{F}' = \mathbf{F}\mathbf{F}_n^{p-1}$$

$$\mathbf{R}^e \mathbf{U}^e \exp\left(\frac{\Delta\gamma}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{N}_e^A \otimes \mathbf{N}_e^A\right) = \mathbf{R}' \mathbf{U}'$$

$$\mathbf{R}^e = \mathbf{R}' \quad ; \quad \mathbf{U}^e \exp\left(\frac{\Delta\gamma}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{N}_e^A \otimes \mathbf{N}_e^A\right) = \mathbf{U}'$$

$$\left. \begin{aligned} \lambda'^A &= \lambda_e^A \exp\left(S^A \frac{\Delta\gamma}{\sqrt{2}\sigma^s}\right) \\ \mathbf{N}'^A &= \mathbf{N}_e^A \end{aligned} \right\} \quad A = 1, 2, 3$$

Coaxiality and
Uniqueness of
Polar Decomposition

Update Equations

$$\varepsilon_e^A = \varepsilon'^A - \Delta\gamma \frac{S^A(\varepsilon_e)}{\sqrt{2}\sigma^s(S)} \quad \varepsilon = \ln(\lambda)$$

$$\Delta\gamma = p(\gamma_n + \Delta\gamma, \sigma^s) \Delta t$$

$$\mathbf{F}^p = \exp\left(\frac{\Delta\gamma}{\sqrt{2}\sigma^s} \sum_A S^A \mathbf{N}'^A \otimes \mathbf{N}'^A\right) \mathbf{F}_n^p$$

$$\mathbf{U}^e = \sum_A \lambda_e^A \mathbf{N}'^A \otimes \mathbf{N}'^A$$

Linearization of Virtual Work

$$R = \int_V \mathbf{T} : \delta \mathbf{L} \, dv = \int_{V_0} \boldsymbol{\tau} : \delta \mathbf{L} \, dv_0 \quad ; \quad \delta \mathbf{L} := \frac{\partial \delta \mathbf{x}}{\partial \mathbf{x}}$$

$$dR = \int_{V_0} d\boldsymbol{\tau} : \delta \mathbf{L} \, dv_0 + \int_V \mathbf{T} : d\delta \mathbf{L} \, dv$$

$$\begin{aligned} d\boldsymbol{\tau} &= \sum_A d\tau^A \mathbf{n}_e^A \otimes \mathbf{n}_e^A + \sum_A \tau^A d(\mathbf{n}_e^A \otimes \mathbf{n}_e^A) \\ &= \sum_A d\tau^A \mathbf{n}'^A \otimes \mathbf{n}'^A + \mathbf{F}' \left\{ \sum_A d \left(\frac{\mathbf{N}'^A \otimes \mathbf{N}'^A}{\mu'^A} \right) \right\} \mathbf{F}'^T + d\mathbf{L}\boldsymbol{\tau} + \boldsymbol{\tau}d\mathbf{L} \quad ; \quad \mu'^A = (\lambda'^A)^2 \end{aligned}$$

Linearization: Geometric Stiffness

(3 distinct e-values of Predictor Stretch)

Serrin, Cayley-Hamilton, Characteristic Equation:
(Simo, 1991)

$$\mathbf{F}' \left\{ \sum_A d \left(\frac{\mathbf{N}'^A \otimes \mathbf{N}'^A}{\mu'^A} \right) \right\} \mathbf{F}'^T = \sum_A \frac{2\tau^A}{D'^A} \left[\begin{array}{l} \mathbf{II}_{B'} - \mathbf{B}' \otimes \mathbf{B}' + \frac{I'_3}{\mu'_A} (\mathbf{I} \otimes \mathbf{I} - \mathbf{II}) \\ + \mu'_A (\mathbf{B}' \otimes \mathbf{m}'^A + \mathbf{m}'^A \otimes \mathbf{B}') \\ + (I'_1 \mu'_A - 4\mu'^2_A + I'_3 \mu'^{-1}_A) \mathbf{m}'^A \otimes \mathbf{m}'^A \\ - \frac{I'}{\mu'_A} (\mathbf{I} \otimes \mathbf{m}'^A + \mathbf{m}'^A \otimes \mathbf{I}) \end{array} \right] : d\mathbf{D}$$

$\mathbf{m}'^A := \mathbf{n}'^A \otimes \mathbf{n}'^A$
 $D'^A := [\mu'^A - \mu'^{A+1}] [\mu'^A - \mu'^{A+2}]$

symmetric

Linearization: Material Stiffness

(3 distinct e-values of Predictor Stretch)

$$\sum_A \delta \mathbf{D} : \mathbf{n}'^A \otimes \mathbf{n}'^A d\tau^A = \delta \mathbf{D} : \left[\sum_A \sum_B (\mathbf{n}'^A \otimes \mathbf{n}'^A) H_B^A (\mathbf{n}'^B \otimes \mathbf{n}'^B) \right] : d\mathbf{D}$$

$$H := \left[\mathbf{A}_A^B + \frac{\Delta\gamma}{\sqrt{2}\tau^s} \left(\delta_A^B - \frac{1}{3} i^A i^B - \frac{1}{2} \left\{ 1 + \frac{\kappa}{\Delta\gamma J \tau^s} \right\} \tau^{dA} \tau^{dB} \right) + \frac{\kappa \sigma^s \tau^{dB}}{\sqrt{2}\tau^s} \sum_C \mathbf{A}_A^C \right]^{-1}$$

$$\kappa := \frac{\Delta t \partial_{\sigma^s} p}{(1 - \Delta t \partial_{\gamma} p)} \quad \text{recall} \quad \dot{\gamma} = p(\gamma, \sigma^s)$$

$$\mathbf{A} := \left[\frac{\partial \tau^A}{\partial \varepsilon^B} \right]^{-1} \quad \leftarrow \text{Nonlinear elasticity (symmetric)}$$

$$i := (1, 1, 1) \quad ; \quad \tau^s = \|\boldsymbol{\tau}^{dev}\| / \sqrt{2} \quad ; \quad \tau^{dA} = A^{th} \text{ e-value of } \boldsymbol{\tau}^{dev}$$

Asymmetry due to Cauchy stress in flow rule

If F^p in flow-rule (e.g. viscoelasticity) then additional asymmetry

Linearization:

Coalescence of e-values of Predictor Stretch

- Geometric Stiffness is ‘highly’ singular in case of 1 or 2 repeated eigenvalues of the Predictor Stretch tensor
- These are not exceptional deformation states (e.g. the undeformed state)
- Perturbation of distinct e-value results (as suggested in Simo, 1990) does not work
- Need separate limit expressions

Linearization: Three repeated e-values of Predictor Stretch

- Finite incremental response is completely elastic
 - i.e. $F^e = F'$

- ‘Approximation’ (perhaps exact!)

$$d\boldsymbol{\tau} = \left\{ B_{diag} - B_{off-diag} \right\} d\mathbf{D} + B_{off-diag} tr(d\mathbf{D}) \mathbf{I} ; B = \begin{bmatrix} \frac{\partial \tau^A}{\partial \varepsilon_e^B} \end{bmatrix}$$

Carlson & Hoger, 1986

Linearization:

2 distinct e-values of Predictor Stretch

- **Material Stiffness from expression for 3 distinct e-values case**
- **Use results from Hill (1978) for Lagrangian spin to derive singularity-free “limit” of geometric stiffness**
 - **Quadratic convergence up to 10^{-9} (nondimensional) for residual**
 - **Residual can be taken down to zero up to round-off**
 - **Expression involves non-unique e-vectors and principal dyads**